

**NL MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7- 6-87	
Company AMOCO			Connection NONE		
Pool FOWLER SILURIAN			Formation SILURIAN		
Completion Date 7/7/87		Total Depth 9900.		Plug Back TD 9740.	
		Elevation 3264.		Farm or Lease Name SOUTH MATTIX UNIT	
Csg. Size 7.000	Wt. 23.0	d 6.366	Set At 9900.	Perforations: From 7002. To 7040.	
Tbg. Size 2.875	Wt. 4.7	d 2.441	Set At 0.	Perforations: From 0. To 0.	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 6849.	
Producing Thru TUBING		Reservoir Temp. °F 129.0 7021.		Mean Annual Temp. °F 60.0	
		Baro. Press. - P _a 13.2		State NEW MEXICO	
L 7021.	H 7021.	G _g 0.718	% CO ₂ 0.21	% N ₂ 3.12	% H ₂ S 0.0
Prover 0.0		Meter Run 4.0		Taps FLANGE	

FLOW DATA							TUBING DATA		CASING DATA		Direction of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw'	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI											
1.	4.03 X 1.500			220.	5.0	48.	1703.	60.	0.		120.0
2.	4.03 X 1.500			230.	18.0	50.	1590.	48.	0.	0.	1.0
3.	4.03 X 1.500			230.	52.0	67.	1487.	50.	0.	0.	1.0
4.	4.03 X 1.500			240.	77.0	40.	1318.	67.	0.	0.	1.0
5.							1122.	40.	0.	0.	1.0

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	10.84	34.15	233.2	1.0117	1.1802	1.0293	455.
2	10.84	66.16	243.2	1.0098	1.1802	1.0303	881.
3	10.84	112.46	243.2	0.9933	1.1802	1.0273	1468.
4	10.84	139.63	253.2	1.0198	1.1802	1.0335	1883.
5.							

NO.	P _f	Temp. °F	T _f	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.35	508.	1.31	0.944	A.P.I. Gravity of Liquid Hydrocarbons	0.0
2.	0.37	510.	1.32	0.942	Specific Gravity Separator Gas	0.718
3.	0.37	527.	1.36	0.948	Specific Gravity Flowing Fluid	XXXXXX
4.	0.38	500.	1.29	0.936	Critical Pressure	662.
5.					Critical Temperature	387.

P _c 1716.2 P _c ² 2945.				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.8312$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.7247$	
NO.	P _f ²	P _w	P _w ²	P _c ² - P _w ²			
1	2570.	1616.	2611.	335.			
2	2251.	1511.	2284.	661.			
3	1772.	1332.	1774.	1171.			
4	1289.	1156.	1337.	1608.			
5							

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3247.$$

Absolute Open Flow 3247. Mcfd @ 15.025 Angle of Slope θ 48.0 Slope, n 0.901

Remarks: _____

Approved By Commission: JUL 10 1987	Conducted By: JOHN WEST	Calculated By: BARBARA WAGNER	Checked By: STEVE WHITE
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