NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [x] Initial [ ] Annual [ ] Special				Test Date: 12-21-72	
Company: Skelly Oil Company		Connection: El Paso			
Pool: Undesignated		Formation: Fusselman		Unit	
Completion Date: 11-12-72	Total Depth: 17,086		Plug Back TD: 17,020	Elevation: 3138 DF	Farm or Lease Name: West Jal Unit
Csg. Size: 3-1/2 / Wt.: 9.9 / d: 2.992 / Set At: 17084			Perforations: From 16,449 To 16,614		Well No.: 1
Tbg. Size: 2-7/8 / Wt.: 6.4 / d: 2.441 / Set At: 14,930			Perforations: From -- To --		Unit: H / Sec.: 20 / Twp.: 25 / Rge.: 36
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 14,930		County: Lea
Producing Thru: Tubing	Reservoir Temp. °F: 216 @ 16,450		Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
16,449	16,449	.595	1.17	1.13	.25	--	6"	Flange

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						4827	60	--	--	
1.	6"	2.750	365	7.7	47	3370	74	--	--	4 hrs.
2.	"	"	353	6.1	53	3238	75	--	--	4 hrs.
3.	"	"	341	4.9	59	3239	71	--	--	4 hrs.
4.	"	"	335	4.0	66	3290	69	--	--	4 hrs.
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	L_{10} Chart $\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	36.99	47.355	6.15	1.013	1.296	1.034	7519
2.	36.99	36.905	6.05	1.007	1.296	1.031	5808
3.	36.99	29.155	5.95	1.001	1.296	1.030	4557
4.	36.99	23.600	5.90	.9943	1.296	1.028	3657
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	.56	507	1.45	.936
2.	.54	513	1.47	.941
3.	.53	519	1.48	.943
4.	.52	526	1.50	.947
5.				

Gas Liquid Hydrocarbon Ratio -- Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons -- Deg.
Specific Gravity Separator Gas .595 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX .719
Critical Pressure 675 P.S.I.A. 671 P.S.I.A.
Critical Temperature 350 R 391 R

P_c 4808 P_c^2 23116.9

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		3547.2	12,582.6	10,534.3
2		3352.2	11,237.2	11,879.7
3		3316.3	10,997.8	12,119.1
4		3346.2	11,197.1	11,919.8
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{23,116.9}{10,534.3}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.19444$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 16,500$

Absolute Open Flow 16,500 Mcfd @ 15.025 | Angle of Slope θ 45° | Slope, n 1.000

Remarks: Due to excessive amounts of water, points did not line up; therefore, a 45° angle was drawn through highest rate of flow making N = 1.000

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
SUPERVISOR DISTRICT I	Joe Banks	Jim Yancy	