

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-24-74	
Company Continental Oil Company			Connection None		
Pool Jalmat			Formation Jalmat		Unit A
Completion Date 10-24-74		Total Depth 3200	Plug Back TD		Elevation
Farm or Lease Name Jack A-20			Well No. 9		
Csg. Size 5 1/2	Wt. 2	d 2830	Set At	Perforations: From Top of pay To 2950	
Tbg. Size 2	Wt.	d	Set At	Perforations: From open end To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At	
Producing Thru		Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. - P _a	
L		H	G _g	% CO ₂	% N ₂
			651 (Assumed)		
				% H ₂ S	Prover
					2"
					Meter Run
					Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI											
1.	2	x	1/8	278		69	287		277		
2.	2	x	3/16	270		70	278		273		30 Min
3.	2	x	7/32	261		69	270		267		30 Min
4.	2	x	1/4	251		70	261		261		45 Min.
5.	2	x	5/16	230		70	251		253		1 hr.
							230		238		1 hr.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	.2648		291.2	.9915	1.239	1.028	99
2	.6082		283.2	.9905	1.239	1.027	217
3	.8393		274.2	.9915	1.239	1.027	290
4	1.087		264.2	.9905	1.239	1.025	361
5	1.672		243.2	.9905	1.239	1.023	510

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	.43	529	1.41	.946	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	.42	530	1.41	.948	Specific Gravity Separator Gas _____
3.	.41	529	1.41	.948	Specific Gravity Flowing Fluid _____ X X X X X
4.	.39	530	1.41	.951	Critical Pressure _____ 670 P.S.I.A.
5.	.36	530	1.41	.956	Critical Temperature _____ 375 R

P _c 300.2	P _c ² 90.1					
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.337$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.337$
1		285.2	81.9	8.2		
2		280.2	78.5	11.6		
3		274.2	75.2	14.9		
4		266.2	70.9	19.2		
5		251.2	63.1	27.0		

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.702$

Absolute Open Flow 1,702 Mcfd @ 15.025	Angle of Slope 45°	Slope, n 1,000
Remarks: No fluid made during test.		

Approved By Commission: <i>John W. Runyan</i>	Conducted By: Reggie Reston	Calculated By: Reggie Reston	Checked By:
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