

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-28-89	
Company Texaco Inc.				Connection None			
Pool West Jal				Formation Strawn		Unit	
Completion Date 12/19/75		Total Depth 18,945		Plug Back TD 12,630		Elevation 3151' KB	
Farm or Lease Name West Jal "B" Deep		Well No. 1					
Csq. Size 7-3/4"	Wt. 46.1	d 6,560	Set At 14,685	Perforations: From 11,708 To 11,995		Unit Sec. Twp. Rge. H 17 25S 36E	
Thg. Size 2 3/8	Wt. 4.7	d 1,995	Set At 11,515	Perforations: From Open To Ended			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 11,496	
Producing Thru Tubing		Reservoir Temp. °F 189 @ 11,511		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
State New Mexico							
L 11,511	H 11,511	G _g .678	% CO ₂ 2.03	% N ₂ .65	% H ₂ S -	Prover	Meter Run 6.065
						Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1922		Pkr.		7 days
1.	6 x 1.750			330	13.00	85	1920		Pkr.		1 hr.
2.	6 x 1.750			345	31.00	100	1875		Pkr.		1 hr.
3.	6 x 1.750			330	46.00	97	1740		Pkr.		1 hr.
4.	6 x 1.750			450	64.00	96	1605		Pkr.		1 hr.
5.	6 x 1.750			730	50.00	98	1522		Pkr.		30 min.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	14.61	66.80	343.2	.9768	1.214	1.033	1.196
2	14.61	105.38	358.2	.9636	1.214	1.031	1.875
3	14.61	125.65	343.2	.9662	1.214	1.030	2.218
4	14.61	172.18	463.2	.9671	1.214	1.041	3.075
5	14.61	192.77	743.2	.9653	1.214	1.066	3.518

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.50	545	1.43	.937	41.2	58.9 @ 60	.678	X X X X X X X X	677	379
2	.52	560	1.47	.940				X X X X X		
3	.50	557	1.46	.942						
4	.68	556	1.46	.923						
5	1.09	558	1.47	.880						

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		2003.6	4014.4	104.5
2		1977.7	3911.3	207.6
3		1967.4	3870.7	248.2
4		1951.1	3806.8	312.1
5		1945.9	3786.5	332.4

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 12.391$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 43.592$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 12.391$

Absolute Open Flow	43,592	Mcfd @ 15.025	Angle of Slope	45	Slope, n	1.000
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Remarks: x = corrected to 2.03% CO₂
Well made 49.0 bbls 58.9 API condensate & 1.5 bbls H₂O

JAN 04 1989

Approved By Division ORIGINAL SIGNED BY JERRY SEXTON DISTRICT SUPERVISOR	Conducted By:	Calculated By: J.B.M.	Checked By: J.B.M.
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