NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-9-80	
Company: Getty Oil Company		Connection: El Paso			
Pool: Wildcat West Jal Atoka		Formation: Atoka			Unit: West Jal "B" Deep
Completion Date: 6-5-80	Total Depth: 18,945	Plug Back TD: 12,870		Elevation: 3171 KB	Farm or Lease Name:
Csg. Size: 7 3/4 / Wt.: 46.1 / d: 6.445 / Set At: 14,685		Perforations: From 12,682 To 12,706			Well No.: 1
Tbg. Size: 3 1/2 / Wt.: 9.3 / d: 2.992 / Set At:		Perforations: From To			Unit: H / Sec.: 17 / Twp.: 25S / Rge.: 36-E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 11,288		County: Lea
Producing Thru: Tubing	Reservoir Temp. °F: 175 @ 12,682	Mean Annual Temp. °F: 60°F	Baro. Press. – P_a: 13.2		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11,308	11,308	.665	.331	1.6	--		4"	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					5850		PKR		S.I.
1.	4.00 x 2"	7.05	4.0	74	5580	74			1.25 hr
2.	4.00 x 2"	7.96	10.89	77	5425	77			1.0 hr
3.	4.00 x 2"	10.32	37.21	77	4875	77			1.5 hr.
4.	4.00 x 2"	13.84	72.25	71	4000	71			1.5 hr.
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	19.81	9.00	20.25	0.9868	1.226	1.001	341
2.	19.81	15.18	21.16	0.9840	1.226	1.001	579
3.	19.81	29.59	23.53	0.9840	1.226	1.001	1,119
4.	19.81	44.20	27.04	0.9896	1.226	1.001	1,681
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	.0303	534	1.432	.998
2.	.0317	537	1.440	.998
3.	.0352	537	1.440	.998
4.	.0405	531	1.424	.998
5.				

Gas Liquid Hydrocarbon Ratio 27.12 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 50.0 Deg.
Specific Gravity Separator Gas .665 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX .7770
Critical Pressure 668 P.S.I.A. 666 P.S.I.A.
Critical Temperature 373 R 415 R

P_c 7572 P_c^2 57,335

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		7,295	53,217	4,117
2		7,129	50,825	6,512
3		6,579	43,285	14,051
4		5,868	34,435	22,901
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 13.93$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 12.53$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 4,274$

Absolute Open Flow 4,274 Mcfd @ 15.025 Angle of Slope θ Slope, n .960

Remarks: Pc & Pw measured

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
Orig. Signed By Jerry Sexton Dist. Supv.	Bill Krafft	H. Terry	Dale Crockett