

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2-3-76			
Company Skelly Oil Company				Connection El Paso Natural Gas					
Pool West Jal Fusselman				Formation Fusselman				Unit	
Completion Date 1-7-76		Total Depth 18945'		Plug Back TD 17065'		Elevation 3140 DF		Farm or Lease Name West Jal "B" Deep	
Csg. Size 5' Liner	Wt. 23.60	d 4.044	Set At 14332'	Perforations: From 16411' To 16439'		Well No. 1			
Tbg. Size 3.5	Wt. 9.30	d 2.992	Set At 14332'	Perforations: From - To -		Unit J	Sec. 17	Twp. 25	Rge. 36
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 14332'		County Lea	
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L 16425	H 16425	Gg .594	% CO ₂ 1.25	% N ₂ 1.71	% H ₂ S -	Prover -	Meter Run 4"	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4		2	290	25"	66	3139	74	Packer		4
2.	4		2	290	36"	62	2808	68			2
3.	4		2	290	45"	62	2316	65			2
4.	4		2	290	52"	62	1506	60			2
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1.	19.8129	87.1	303.2	.9943	1.297	1.023	2276
2.	19.8129	104.5	303.2	.9981	1.297	1.024	2744
3.	19.8129	116.8	303.2	.9981	1.297	1.024	3068
4.	19.8129	125.6	303.2	.9981	1.297	1.024	3298
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.45	526	1.52	.956			.594			
2.	.45	522	1.50	.954						
3.	.45	522	1.50	.954						
4.	.45	522	1.50	.954						
5.										

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.	3155.7	9958.5	17627	
2.	2827.5	7994.6	19591	
3.	2340.4	5477.6	22108	
4.	1536.3	2360.3	25225	
5.				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.56$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3606$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.56$

Absolute Open Flow	3606	Mcfd @ 15.025	Angle of Slope θ	45.0	Slope, n	1.000
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Remarks:

Approved By Commission:	Conducted By: Joe Banks	Calculated By: Jerrel Harburger	Checked By:
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