

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 6-30-83	
Company AMOCO PRODUCTION COMPANY				Connection ATMOSPHERE	
Pool UND				Formation STRAWN	
Completion Date 2 7 83		Total Depth 16190.		Plug Back TD 14217.	
Elevation 3165.		Farm or Lease Name FEDERAL DD			
Chp. Size 2.875	Wt. 6.5	d 2.441	Set At 14268.	Perforations: From 13766. To 14176.	
Well No. 1					
Thp. Size 2.875	Wt. 6.5	d 2.441	Set At 12991.	Perforations: From 0. To 0.	
Unit 34	Sec. 25	Twp. 35	Rge.		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 12082.	
Producing Thru TUBING		Reservoir Temp. °F 180.0 13971.		Mean Annual Temp. °F 60.0	
Baro. Press. - P _g 13.2		State NEW MEXICO			
L 13971.	H 13971.	C _g 0.670	% CO ₂ 0.23	% N ₂ 1.00	% H ₂ S 0.
Praver 2.0	Meter Run 0.	Taps.			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Power Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							4855.	50.			384.0
1.	2.00 X 1.250			5.	0.	61.	3522.	61.	0.	0.	1.0
2.	2.00 X 1.250			10.	0.	42.	2230.	42.	0.	0.	0.7
3.	2.00 X 1.250			24.	0.	44.	1373.	44.	0.	0.	0.7
4.	2.00 X 1.250			32.	0.	58.	700.	58.	0.	0.	0.7
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	27.57	0.	13.2	0.9990	1.2220	1.0018	614.
2	27.57	0.	23.2	1.0178	1.2220	1.0027	798.
3	27.57	0.	37.2	1.0157	1.2220	1.0043	1279.
4	27.57	0.	45.2	1.0019	1.2220	1.0047	1533.
5							

NO.	P _g	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1	0.03	521.	1.38	0.996	A.P.I. Gravity of Liquid Hydrocarbons _____ 51.5 _____ Deg.
2	0.03	502.	1.33	0.995	Specific Gravity Separator Gas _____ 0.670 _____
3	0.06	504.	1.34	0.992	Specific Gravity Flowing Fluid _____ X X X X X _____
4	0.07	518.	1.37	0.991	Critical Pressure _____ 668. _____ P.S.I.A. _____ 651. _____ P.S.I.A.
5					Critical Temperature _____ 377. _____ R _____ 487. _____ R

P _c 4893.3 P _c ² 23945.				
NO.	P _c ²	P _w	P _w ²	P _c ² - P _w ²
1	12498.	3541.	12542.	11402.
2	5032.	2307.	5323.	18622.
3	1922.	1476.	2178.	21767.
4	509.	727.	529.	23416.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0226$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0226$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1568.$

Absolute Open Flow _____ 1568. _____ Mcfd @ 15.025

Angle of Slope θ _____ 45.0 _____ Slope, n _____ 1.000

Remarks: _____

Approved By Commission:	Conducted By: WINN SUTTON W/JOHN WEST ENGINEERING	Calculated By: STEVE BATES W/AMOCO	Checked By: STEVE WHITE W/AMOCO
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RECEIVED

JUN 8 1983

O.C.D.
HOBS OFFICE