

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 09-26-90									
Company Oryx Energy Co.		Connection 9-18-90 Transwestern Pipeline Co.									
Pool Wildcat		Formation Atoka									
Completion Date 7-18-90		Total Depth 15,700'	Plug Back TD 15,050'								
		Elevation 3442.6' GR	Farm or Lease Name Gila 4 Deep Com								
Csq. Size 4 1/2"	Wt. 15.10#	Set At 15,698'	Perforations: From 14,276' To 14,334'								
Thq. Size 2 7/8"	Wt.	Set At 14,176'	Perforations: From To								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 14,176'	Well No. 1								
Producing Thru	Reservoir Temp. °F #	Mean Annual Temp. °F	Baro. Press. - P _a								
L 14305	H 14305	G _g .651	% CO ₂ 1.03								
		% N ₂ .71	% H ₂ S .00								
		Prover .0	Meter Run 4.0								
			Taps Flange								
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							7280	75			24.0
1.	4.03	X	2.000	170	14.0	82	6920	74	0.	0.	1.0
2.	4.03	X	2.000	300	20.0	93	6795	75	0.	0.	1.0
3.	4.03	X	2.000	450	46.0	81	6180	75	0.	0.	1.0
4.	4.03	X	2.000	750	65.0	56	5245	75	0.	0.	1.0
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	19.81	50.64	183.2	.9795	1.2389	1.0154	1237				
2	19.81	79.15	313.2	.9697	1.2389	1.0248	1931				
3	19.81	145.97	463.2	.9804	1.2389	1.0403	3655				
4	19.81	222.73	763.2	1.0039	1.2389	1.0822	5940				
5											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 241.666 Mcf/bbl.						
1	.27	542	1.46	.970	A.P.I. Gravity of Liquid Hydrocarbons 48.5						
2	.47	553	1.49	.952	Specific Gravity Separator Gas .651						
3	.69	541	1.46	.924	Specific Gravity Flowing Fluid .663						
4	1.13	516	1.39	.854	Critical Pressure 673. P.S.I.A.						
5					Critical Temperature 371 R						
$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{7278.1}{52970.}$					$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{2.1404}{1.9973}$						
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 11200$											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²							
1		6922	47913	5057							
2		6799	46233	6737							
3		6203	38474	14496							
4		5312	28222	24748							
5											
Absolute Open Flow 11200 Mcfd @ 15.025					Angle of Slope 49°		Slope, n .869				
Remarks:											
OCT 15 1990											
Approved By Commission:			Conducted By:			Calculated By:		Checked By:			
ORIGINAL FILED BY JERRY SEXTON			<i>[Signature]</i>								