

Submit in duplicate to
appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

Form C-122
Revised October, 1999

Oil Conservation Division
1220 South St. Francis Dr.
Santa Fe, NM 87504

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator E.O.G. Resources, Inc.						Lease or Unit Name Triste Draw "3" Fed					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-31-01		Well No. 3			
Completion Date		Total Depth 13920		Plug Back TD 13845		Elevation		Unit Ltr. - Sec. - TWP - Rge. P 3-25-33			
Csg. Size	Wt.	d	Set At	Perforations:				County Lea			
Thg. Size	Wt.	d	Set At	Perforations:				Pool Johnson Ranch			
2 7/8		6.5		2.441		13913		From: 13620 To: 13670		Formation Wolfcamp	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At None		Connection Wolfcamp			
Producing Thru Tbg		Reservoir Temp. °F		Mean Annual Temp. °F 60		Baro. Press - P. 13.2		Mejer Run 4.026			
L 13620		H 13620		Gg .645	%CO ₂ .525	%N ₂ .683	%H ₂ S	Prover	Taps Flg		

FLOW DATA					TUBING DATA		CASING DATA		Duration Of Flow	
No.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI						1382		N/A		48 HRS
1.	4 X	1.875	269			1298		N/A		1 HR
2.	4 X	1.875	273			1220		N/A		1 HR
3.	4 X	1.875	280			1095		N/A		1 HR
4.	4 X	1.875	253			986		N/A		1 HR
5.										

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.							307
2.			Metered by	Total Flow			466
3.							647
4.							836
5.							

No.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.					A. P. I. Gravity of Liquid Hydrocarbons	Dry	Deg.
2.		N/A			Specific Gravity Separator Gas	.645	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX	
4.					Critical Pressure	670	P.S.I.A. P.S.I.A.
5.					Critical Temperature	372	R. R.

No.	P _i ²	P _w	P _w ²	P _e ² - P _w ²	(1) P _{e2} = $\frac{P_e^2 - P_w^2}{P_e^2 - P_w^2}$	(2) $\left[\frac{P_e^2}{P_e^2 - P_w^2} \right]^n =$
1.		1311.7	1720.6	226.0	2.075	1.669
2.		1234.4	1523.9	422.7		
3.		1110.9	1234.1	712.5		
4.		1004.3	1008.6	938.0		
5.						

Absolute Open Flow 1,396 Mcfd@ 15.025		Angle of Slope θ: 54.9		Slope, n: .7020	
Remarks: No Fluid Produced					
Approved By Division		Conducted By: Signal Wireline		Checked By: BM	

EOG RESOURCES, INC.
TRISTE DRAW "3" FEDERAL # 3

