

## NEW MEXICO OIL CONSERVATION COMMISSION

MODES OFFICE OCC

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Jalmat Formation Yates County Lea  
Initial \_\_\_\_\_ Annual \_\_\_\_\_ Special X Date of Test 12-31-56 = 1-4-57  
Company King, Warren & Dye Lease Toby Well No. 2  
Unit K Sec. 7 Twp. 24S Rge. 37E Purchaser EPNG  
Casing 5 1/2 Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at 3423 Perf. 2910 To 3030  
Tubing 2 Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at \_\_\_\_\_ Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 2910 To 3030 L 2910 xG .655 -GL 1906 Bar.Press. 13.2  
Producing Thru: Casing \_\_\_\_\_ Tubing \_\_\_\_\_ Type Well G.O. Dual  
Date of Completion: 7-25-47 Packer No Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. \_\_\_\_\_

## OBSERVED DATA

Tested Through (Prover) (Choke) (Meter)

Type Taps \_\_\_\_\_

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI										
1.	4	2,000	846	4.41	89			892		72
2.	4	2,000	826	9.61	85			855		24
3.	4	2,000	774	27.56	80			839		24
4.	4	2,000	690	69.72	76			794		24
5.								721*		24

\*Not enough draw down - choke restriction

## FLOW CALCULATIONS

No.	Coefficient Fig. (24-Hour)	$\sqrt{h_w P_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	25.58	61.55		.9732	.9371	1.077	1,579
2.	25.58	89.79		.9768	.9371	1.077	2,313
3.	25.58	147.28		.9813	.9371	1.072	3,793
4.	25.58	221.39		.9850	.9371	1.070	5,713
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> 1.712 (1-e<sup>-s</sup>) .123

Specific Gravity Separator Gas \_\_\_\_\_  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 905.2 P<sub>c</sub> 819.4

No.	$\frac{P_w}{P_t}$ (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	$\frac{(F_c Q)^2}{(1-e^{-s})}$	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	$\frac{P_w}{P_c}$
1.	868.2	753.8	2.70	7.29	.9	754.7	64.7	868.7	.96
2.	852.2	726.2	3.96	15.68	1.9	728.1	91.3	853.3	.94
3.	807.2	651.6	6.49	42.12	5.2	656.8	162.6	810.4	.90
4.	734.2	539.0	8.78	95.65	11.8	550.8	268.6	742.2	.82
5.									

Absolute Potential: 14,800 MCFPD; n .839COMPANY El Paso Natural Gas Co.ADDRESS Box 1492, El Paso, Texas

AGENT and TITLE \_\_\_\_\_

WITNESSED Test conducted by Edward MabeCOMPANY El Paso Natural Gas Company

REMARKS \_\_\_\_\_

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .