

## NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE 066 Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

1157 NOV 20 AM 10 14 Revised 12-1-55

Pool Jalmat Formation Yates County Lea  
Initial \_\_\_\_\_ Annual \_\_\_\_\_ Special XX Date of Test 12-31-56/1-4-57  
Company Skelly Oil Company Lease Lib. Royalties Well No. 5  
Unit J Sec. 7 Twp. 24 S Rge. 37 E Purchaser El Paso Natural Gas Company  
Casing 5 1/2" Wt. 14 1/2 I.D. 5.012" Set at 2730 Perf. \_\_\_\_\_ To \_\_\_\_\_  
Tubing None Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at \_\_\_\_\_ Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 2730' To 3240' L 2730 xG 0.650 -GL 1775 Bar.Press. 13.2  
Producing Thru: Casing XX Tubing \_\_\_\_\_ Type Well Single  
Single-Bradenhead-G. G. or G.O. Dual  
Date of Completion: 1-4-49 Packer None Reservoir Temp. \_\_\_\_\_

## OBSERVED DATA

Tested Through (PROPER) (ORIFICE) (Meter)

Type Taps \_\_\_\_\_

| Flow Data |                              |                                  |        |                | Tubing Data |        | Casing Data |        | Duration<br>of Flow<br>Hr. |       |
|-----------|------------------------------|----------------------------------|--------|----------------|-------------|--------|-------------|--------|----------------------------|-------|
| No.       | ( <del>PROPER</del> ) (Line) | ( <del>ORIFICE</del> ) (Orifice) | Press. | Diff.          | Temp.       | Press. | Temp.       | Press. |                            | Temp. |
|           | Size                         | Size                             | psig   | h <sub>w</sub> |             | °F.    | psig        | °F.    |                            | psig  |
| SI        |                              |                                  |        |                |             |        |             | 909    |                            | 72    |
| 1.        | 4                            | 2.000                            | 855    | 9.61           | 96          |        |             | 864    |                            | 24    |
| 2.        | 4                            | 2.000                            | 808    | 25.00          | 89          |        |             | 829    |                            | 24    |
| 3.        | 4                            | 2.000                            | 772    | 39.69          | 86          |        |             | 802    |                            | 24    |
| 4.        | 4                            | 2.000                            | 719    | 82.81          | 81          |        |             | 754 *  |                            | 24    |
| 5.        |                              |                                  |        |                |             |        |             |        |                            |       |

\* Not enough draw down - orifice too small.

## FLOW CALCULATIONS

| No. | Coefficient<br>(24-Hour) | $\sqrt{h_{wP_f}}$ | Pressure<br>psia | Flow Temp.<br>Factor<br>F <sub>t</sub> | Gravity<br>Factor<br>F <sub>g</sub> | Compress.<br>Factor<br>F <sub>pv</sub> | Rate of Flow<br>Q-MCFPD<br>@ 15.025 psia |
|-----|--------------------------|-------------------|------------------|--|-------------------------------------|--|--|
| 1.  | 25.58                    | 91.33             |                  | 0.9671                                 | 0.9608                              | 1.073                                  | 2,328                                    |
| 2.  | 25.58                    | 143.27            |                  | 0.9732                                 | 0.9608                              | 1.074                                  | 3,681                                    |
| 3.  | 25.58                    | 176.51            |                  | 0.9759                                 | 0.9608                              | 1.070                                  | 4,529                                    |
| 4.  | 25.58                    | 246.20            |                  | 0.9804                                 | 0.9608                              | 1.066                                  | 6,325                                    |
| 5.  |                          |                   |                  |  |                                     |  |  |

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> 0.9002 (1-e<sup>-s</sup>) 0.115

Specific Gravity Separator Gas \_\_\_\_\_  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 922.2 P<sub>c</sub> 850.5

| No. | P <sub>w</sub><br>P <sub>t</sub> (psia) | P <sub>t</sub> <sup>2</sup> | F <sub>c</sub> Q | (F <sub>c</sub> Q) <sup>2</sup> | (F <sub>c</sub> Q) <sup>2</sup><br>(1-e <sup>-s</sup> ) | P <sub>w</sub> <sup>2</sup> | P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup> | Cal.<br>P <sub>w</sub> | P <sub>w</sub><br>P <sub>c</sub> |
|-----|---|-----------------------------|------------------|---------------------------------|---|-----------------------------|--|------------------------|----------------------------------|
| 1.  | 877.2                                   | 769.5                       | 2.10             | 4.41                            | 0.51  | 770.0                       | 80.5   |                        |                                  |
| 2.  | 842.2                                   | 709.3                       | 3.31             | 10.96                           | 1.26  | 710.6                       | 139.9  |                        |                                  |
| 3.  | 815.2                                   | 664.6                       | 4.08             | 16.65                           | 1.91  | 666.5                       | 184.0  |                        |                                  |
| 4.  | 767.2                                   | 588.6                       | 5.69             | 32.38                           | 3.72  | 592.3                       | 258.2  |                        |                                  |
| 5.  |   |                             |                  |                                 |   |                             |  |                        |                                  |

Absolute Potential: 15,900 MCFPD; n 0.812COMPANY Skelly Oil CompanyADDRESS Box 38, Hobbs, New Mexico

AGENT and TITLE \_\_\_\_\_

WITNESSED \_\_\_\_\_

COMPANY \_\_\_\_\_

REMARKS

ELVIS A. H.  
GAS ENGINEER

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .