## NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE FORE C-122
1957 NOV EDREY; sed 12-1-55

						- %
MULTI-POINT	BACK	PRESSURE	TEST	FOR	GAS	WELLS

	Jalmat			_Formation	Yates			County	Lea	<sup>10</sup> 14
										-31-56/1-4-57
										3
										- Company
	ng None									
Prod	Pay: From	Cacin	YY		<u>.                                    </u>	U.BSU	GL1	775	Bar.Pre	355. 42.4
not -	ucing Thru	ı. Casır		ru	onng,	Sin	Type we gle-Brade	enhead-G.	G. or (	G.O. Dual
Date	of Comple	etion: <u>1-</u>	4-49	Packe	r None		Reservo	oir Temp		
					OBSERVI	ED DATA				
Test	ed Through	XXXXX	<u> </u>	(Meter)				Type Tap	s	
			w Data		T	Tubing	Data	Casing Da	ata	<u> </u>
		LIMITE		s. Diff.	Temp.		Temp.	Press.	Temp.	Duration
No.	(Line) Size	(Orific	7	g h <sub>w</sub>	o <sub>F</sub> .	psig	°F.	psig	<sup>⊃</sup> F•	of Flow Hr.
SI	<del></del>		<del>-  </del>	<del>- "</del>		16				72
		2,000	855	9.51	96		_ <del></del>	909 864		24
1. 2.		2.000	808	25.00	89	<del></del>		829		24
3.		2.000	772	39.69	86			802		24
4. 5.		2,000	719		n			754 *		24
	Coeffic			Pressure	FLOW CALC	Cemp.	Gravity	Compres   Factor		Rate of Flow Q-MCFPD
No.		ŀ			ract	,01	Factor	ractor		Q-MOTPD
No.	(24-Ho	ur) $$	h <sub>w</sub> p <sub>f</sub>	psia	F <sub>t</sub>		$^{\mathrm{F}}g$	$\mathbf{F}_{\mathbf{p}\mathbf{v}}$		@ 15.025 psia
	25.58		1.33	psia	F <sub>t</sub>	; <u> </u>	F <sub>g</sub> 0.960 <b>6</b>	F <sub>pv</sub>		@ 15.025 psia <b>2,325</b>
	25.58 25.58	1	3.27	psia	F <sub>t</sub> 0.9671 0.9732		0.960 <b>6</b> 0.960 <b>6</b>			@ 15.025 psia 2,328 3,681
	25.58 25.58 25.58		1.33 3.27 6.51	psia	F <sub>t</sub> 0.9671 0.9732 0.9759	,	0.760 <b>6</b> 0.760 <b>8</b> 0.760 <b>8</b>	1.073 1.074 1.070		@ 15.025 psia 2,328 3,681 4,529
	25.58 25.58		3.27	psia	F <sub>t</sub> 0.9671 0.9732	,	0.960 <b>6</b> 0.960 <b>6</b>	1.073		@ 15.025 psia 2,328 3,681
1. 2. 3. 4. 5. as Li	25.58 25.58 25.58 25.58 25.58	ocarbon R	1.33 3.27 76.51 6.20 atio_arbons		F <sub>t</sub> 0.9671 0.9732 0.9759 0.9804  CSSURE CA		0.3608 0.9608 0.9608 0.9608 0.9608 0.9608	1.073 1.076 1.070 1.066	y Sepa	@ 15.025 psia 2,328 3,681 4,529 6,325  rator Gas_ ing Fluid
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1. 2. 3. 4. 5. 5. No. No. 2.	25.58 25.58 25.58 25.58 25.58 25.58 25.58 25.58 25.58 27.20 27.20 27.20 27.20	Pt 769.5	1.33 3.27 76.51 6.20 arbons (1-e-s	PRE  (F <sub>c</sub> Q) <sup>2</sup> 4.41	Ft 0.9671 0.9732 0.9759 0.9804  CSSURE CA cf/bbl. deg.  (Fc (1- 0.5	Q) <sup>2</sup> e <sup>-s</sup> )	0.3608 0.9608 0.9608 0.9608 0.9608 0.9608 0.9608 0.9608 0.9608 0.9608 0.9608	1.073 1.074 1.070 1.066 fic Gravit fic Gravit 2.2 P <sub>c</sub> -P <sub>w</sub> <sup>2</sup> 80.5 139.9	y Sepa y Flow Pc 85	@ 15.025 psia 2,328 3,681 4,529 6,325  rator Gas ing Fluid 0.5
1. 2. 3. 4. 5. 1. No. 1. 2. 3.	25.58 25.58 25.58 25.58 26.58 27.2 28.2 29.502 29.502	Pt 769.5	1.33 3.27 76.51 6.20 arbons _(1-e <sup>-5</sup> ) F <sub>c</sub> Q 2.10 3.31	PRE  (F <sub>c</sub> Q) <sup>2</sup> 4.41  10.96  6.65	Ft 0.9671 0.9732 0.9759 0.9804  CSSURE CA  cf/bbl. deg.  (Fc (1- 0.5 1.2	Q) <sup>2</sup> -e <sup>-s</sup> )	0.7608 0.7608 0.7608 0.9608 0.9608 ONS Speci Pc_92 Pw <sup>2</sup> 70.0 10.6	1.073 1.074 1.070 1.066 fic Gravit fic Gravit 2.2 P <sub>c</sub> -P <sub>w</sub> <sup>2</sup> 80.5 139.9	y Sepa y Flow Pc 85	@ 15.025 psia 2,328 3,681 4,529 6,325  rator Gas ing Fluid 0.5
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1. 2. 3. 4. 5. No. 1. 2. 3. 4. 5. Absol COMPA ADDRE	25.58 25	Pt 769.5 709.3 664.6 588.6 2121: 15	Atio_arbons_(1-e <sup>-5</sup> )  F <sub>c</sub> Q  2.10  3.31  4.08  5.69	PRE  (F <sub>c</sub> Q) <sup>2</sup> 1.41  0.96  6.65	Ft 0.9671 0.9732 0.9759 0.9804  CSSURE CA cf/bbl. deg.  (Fc (1- 0.5 1.2 1.9	Q) <sup>2</sup> -e <sup>-s</sup> )	0.7608 0.7608	1.073 1.074 1.070 1.066 fic Gravit fic Gravit 2.2 P <sub>c</sub> -P <sub>w</sub> <sup>2</sup> 80.5 139.9	y Sepa y Flow Pc 85	@ 15.025 psia 2,328 3,681 4,529 6,325  rator Gas ing Fluid 0.5
1. 2. 3. 4. 5. No. 1. 2. 3. 4. 5. Absol COMPA ADDRE	25.58 25	Pt 769.5 709.3 664.6 588.6 2121: 15	Atio_arbons_(1-e <sup>-5</sup> )  F <sub>c</sub> Q  2.10  3.31  4.08  5.69	PRE  (F <sub>c</sub> Q) <sup>2</sup> 1.41  0.96  6.65	Ft 0.9671 0.9732 0.9759 0.9804  CSSURE CA cf/bbl. deg.  (Fc (1- 0.5 1.2 1.9	Q) <sup>2</sup> -e <sup>-s</sup> ) 1 7 1 6 7	0.7608 0.7608	1.073 1.074 1.070 1.066 fic Gravit fic Gravit 2.2 P <sub>c</sub> -P <sub>w</sub> <sup>2</sup> 80.5 139.9	y Sepa y Flow Pc 85	@ 15.025 psia 2,328 3,681 4,529 6,325  rator Gas ing Fluid 0.5

REMARKS

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## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure ( $P_W$ ). MCF/da. @ 15.025 psia and 60° F.
- PcI 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- $P_f$  Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- $F_{pv}$  Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_{\rm W}$  cannot be taken because of manner of completion or condition of well, then  $P_{\rm W}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\rm t}$ .