				NEW	MEXICO	OIL CONS	ERVATIO	N COMmassi	.OM	HOBBS C	١.,	
									1957	750 D	Fiform C-122 evised 9661-55	
				MULTI-	-POINT B	ACK PRES	SURE TE	ST FOR GAS	WELLS	E G	Ph -	
Poo	l Jalmat	<u> </u>		F	ormation	Yate	8 <del>2</del> 7	Rivers	_County	<u> </u>	PH 3:57	
Ini	tial		Annu	al		Spec	ial	_х	_Date of '	Test_4-2	4 to 4-28-15	
Com	pany Johr	) H.	Kelly	·		Lease	Ha	ir	Wel	l No	_1	
Uni	t <u>1</u> S	Sec	8_Tw	p. 24	Rg	e. <u>37</u>	Pur	chaser <u>E</u>	1 Paso N	atural	Gas	
Cas	ing 7" W	/t2	<u>0#</u> _I	.D	Se	t at_ <b>2</b> 8	<b>36</b> P	erf		Го		
Tubing 2 3/8 Wt. 4.7 I.D. Set at 3528 Perf. To												
Gas	Pay: From_	2562	To	3054	L28	62 2	(G <u>. 650</u>		1860	Bar.Pres	s. <u>13.2</u>	
											O. Dual	
Date	e of Complet	ion:	8 <b>-1</b> 8	-52	Packe	r_ 314	Si <b>5</b>	ngle-Br te Reservo	enhead-G. ( oir Temp.	3. or G.(	O. Dual	
	-	_					ED DATA					
Tes	ted Through	(-Prop	warely (	destable.	(Meter)				Type Tan	s Flan	ge	
			Flow Da		<u> </u>		Tubin	g Data	Casing Da			
	(Remera)	(12)m	STREET, X	Press.	Diff.	Temp.	Press	. Temp.	Press.	Temp.	Duration	
No.	(Line) Size	(Ori	fice) ize	psig	h	$o_{\mathrm{F}}$ .	psig	o <sub>F</sub> ,	psig	o <sub>F</sub> .	of Flow Hr.	
SI				P 0	w		18		902		72	
1. 2. 3. 4. 5.	Ą	1.	750	522	15.8	70			785		24	
2.	4	7.	750	526					773		24	
3.	4		750	518		71			744		24	
4.	4	1.	750	535	54.76	68	ļ	_	702		24	
<u> </u>		<u> </u>		Ļ	L				<u></u>			
	Coeffici		ent.		Pressure		CULATIO Temp.	NSGravity	Compre	ss. Ra	ate of Flow	
No.	00011101			` `	Fressure		tor	Factor			-MCFPD	
	(24-Hou	ır) $\sqrt{h_W}$		0.6	psia		t	Fg	,		15.025 psia	
<del></del>		· · · · · · · · · · · · · · · · · · ·			1				PV			
- <del>1</del> .	19.27		94.			.9905 .9905		<u>.9608</u>	1,05		1835	
<del>-2.</del>						•989 •989		<u> 9608</u>	1.05		2373 2814	
7.			140.			-992		9608 -9608	1.05		3354	
1. 2. 3. 4. 5.	19.27		1/0.									
					PR.	ESSURE C	CALCULAT	IONS				
Gas ]	Liquid Hydro	carbo	n Ratio	0		cf/bbl.	ı		fic Gravi			
Grav:	ity of Liqui	d Hyd				deg.	,	Speci	fic Gravi	ty_Flowin	ng Fluid	
Fc	.740		()	l-e <sup>-s</sup> )_	0.120		••	Pc	915.2	_Pc <u>83</u>	7.6	
	ž <sub>n</sub>		2 _		(n a)2	/-	0\2	F. 0	$P_c^2 - P_w^2$	0-3	D	
No.	Pt (psia)	P	t   F	cQ	$(F_cQ)^2$	(1)	$\left(\frac{1}{16}\right)^{2}$	$P_{w}^{2}$	Pc-Pw	Cal P <sub>w</sub>	• P <sub>w</sub> P <sub>c</sub>	
1.	798.2	637.	1 1.	356	139		21	637.3	200.3	798.3	.7	
1. 2.	786.2	2 618.1		760	3.098		72	618.5	219.1	786.4	-86	
3.	757.2			082	4.335	.5	20	573.9	263.7	757.6	•8 <b>3</b>	
4.	715.2	715.2 511.5		482	6.160		39	512.2	325.4	715.7	-7€	
5.					<del></del>		l		<u> </u>	<u></u>		
Abs	olute Potent	ial:	7.	600		MCFPD;	n •	୫ <b>69</b>				
COM	PANY Jo	n_⊮•	Kell	У								
	RESS I or	x 567	14 FO	awell,	New	97/00					<del></del>	
AGENT and TITLE Yeuret WM Your Production Superintendent WITNESSED 1.1. Perby												
	NESSED FANY	- 6	COY SET	ral G	A 8							
OOM	T-1211 T-1		.1 62 0 14									

REMARKS

ILLEGIBLE

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 60° F.
- $P_c$ = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- $P_{w}$  Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- $F_{t}$  Flowing temperature correction factor.
- $F_{pv}$  Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_W$  cannot be taken because of manner of completion or condition of well, then  $P_W$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_+$ .