

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 04/10/80	
Company AMOCO PRODUCTION COMPANY				Connection EL PASO NATURAL GAS COMPANY	
Pool FOWLER PADDOCK				Formation UPPER PADDOCK	
Completion Date 10/11/79		Total Depth 6400.		Plug Back TD 6350.	
Elevation 3246.		Form or Lease Name SOUTH MATTIX UNIT			
Csg. Size 7.000	Wt. 20.0	d 6.456	Set At 6400.	Perforations: From 4846. To 4901.	
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 4816.	Perforations: From 0. To 0.	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple DUAL				Packer Set At 4809.	
Producing Thru TUBING		Reservoir Temp. °F 91. # 4874.		Mean Annual Temp. °F 60.0	
Baro. Press. - P _a 13.2		State NEW MEXICO			
L 4874.	H 4874.	G _g 0.680	% CO ₂ 1.10	% N ₂ 1.55	% H ₂ S 0.
Prover 0.		Meter Run 4.0		Taps FLANGE	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1054.	67.			44.0
1.	4.03 x 2.500			70.	4.0	58.	1005.	72.	0.	0.	1.0
2.	4.03 x 2.500			82.	13.0	33.	913.	77.	0.	0.	1.0
3.	4.03 x 2.500			102.	31.4	35.	693.	82.	0.	0.	1.0
4.	4.03 x 2.500			120.	37.2	57.	468.	85.	0.	0.	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	32.64	18.24	83.2	1.0019	1.2127	1.0087	730.
2	32.64	35.13	95.2	1.0270	1.2127	1.0117	1445.
3	32.64	60.11	115.2	1.0249	1.2127	1.0141	2473.
4	32.64	70.40	133.2	1.0029	1.2127	1.0142	2834.
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NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1	0.12	518.	1.37	0.983	0.	
2	0.14	493.	1.31	0.977	0.	
3	0.17	495.	1.31	0.972	0.680	X X X X X X X X
4	0.20	517.	1.37	0.972	X X X X X	0.680
5					671.	671. P.S.I.A.
					377.	377. R

P _c 1064.8		P _c ² 1134				
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	1037.	1018.	1037.	96.	1.4692	1.2838
2	858.	939.	881.	252.		
3	499.	768.	590.	544.		
4	232.	602.	362.	772.		
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$$AOP = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3639.$$

Absolute Open Flow **3639.** Mcfd @ 15.025 Angle of Slope θ **57.0** Slope, n **0.649**

Remarks: _____

Approved By Commission: 	Conducted By: John West Engr.	Calculated By: R.M. Whitten	Checked By: W. D. Magness
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